Simulation of relativistic outflows in astrophysics

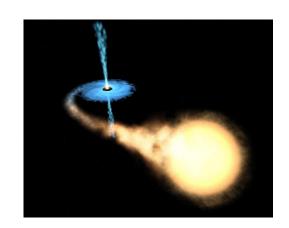
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Plan of Talk



- A short introduction on relativistic flow & Equation of State.
- A brief look on the code.
- Relativistic outflows.
- Concluding Remarks.

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- It is important to use correct γ , influences the value of $c_s \Rightarrow$ would affect T distribution, as well as structure propagations: Are we equipped to do so?

• The equations of motion are (c = 1):

$$(\rho u^{\nu})_{;\nu} = 0, \qquad T^{\mu\nu}_{;\nu} = 0$$

ho, u^{μ} are proper density and 4-velocity, $T^{\mu\nu}=\rho h u^{\mu}u^{\nu}+pg^{\mu\nu}$; h= specific enthalpy $=(e+p)/\rho$, e total proper energy density and p pressure.

Number of eqs = 5; Number of variables = 6.

- To resolve, one assumes an EoS *i.e.*, $h\equiv h(p,\rho)$ or $e\equiv e(p,\rho)$.
- In non-relativistic regime the internal energy density is given by

$$e_{int} = \frac{p}{(\gamma - 1)}$$

the most favoured EoS in RHD is (hereafter ID) is

$$h = 1 + \frac{\gamma \Theta}{\gamma - 1}, \quad \text{or} \quad e = \rho + \frac{p}{\gamma - 1}$$

 $\Theta = p/\rho$ a temperature like variable.

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- ullet (a) In ID γ or n has no temperature dependence
 - (b) Gives unphysical wave speeds!
- Are we free to use any other arbitrary EoS?

Relativistic kinetic theory imposes a strong constrain on EoS, known as Taub's inequality,

$$(h-\Theta)(h-4\Theta)\geq 1$$

• ID do not satisfy TAUB's inequality (TI) for all values of Θ and $\gamma \Rightarrow$ ID is relativistically wrong!

 Chandrashekhar (1934), Synge (1957) calculated the exact EoS for simple gas (RP)

$$h = \frac{K_3(1/\Theta)}{K_2(1/\Theta)},$$

 K_2 and K_3 are modified Bessels function of second kind & of order 2 & 3.

- This accuracy comes at expense of extra computational cost as shown by Falle & Komissarov (1996)! ⇒ Not suitable for Numerical RHD!
- What do we do? Try and propose a new equation of state

New EoS

- New EoS must satisfy:
 - (a) Taub's Inequality for all Θ !
 - (b) Should give $\gamma \to 5/3$ (or $n \to 3/2$) for $\Theta \to 0$ & $\gamma \to 4/3$ (or $n \to 3$) $\Theta \to \infty$!
 - (c) Good fit to RP!

New EoS

Our proposed EoS (RC) is,

$$\frac{p}{e-\rho} = \frac{3p+2\rho}{9p+3\rho}; \quad \text{or} \quad h = 2\frac{6\Theta^2 + 4\Theta + 1}{3\Theta + 2}.$$
 (iv)

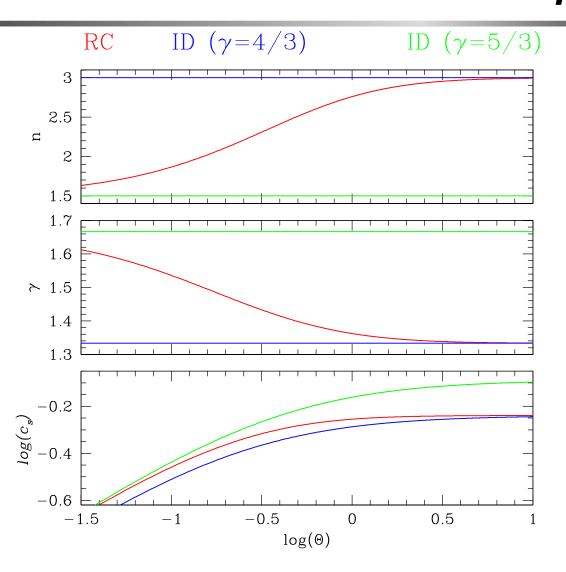
• Expression of $n \& c_s$ with RC EoS:

$$n = 3\frac{9\Theta^2 + 12\Theta + 2}{(3\Theta + 2)^2},$$
 $c_s^2 = \frac{\Theta(3\Theta + 2)(18\Theta^2 + 24\Theta + 5)}{3(6\Theta^2 + 4\Theta + 1)(9\Theta^2 + 12\Theta + 2)}.$

RC is extremely accurate!

$$\frac{|h_{\rm RP} - h_{\rm RC}|}{h_{\rm RP}} \lesssim 0.8\%$$

New EoS



Comparing various quantities top to bottom (i) n, (ii) γ , (iii) c_s ; for RC, ID($\gamma = 4/3$),

$$ID(\gamma = 5/3).$$

Highlights of the new code

- We have implemented RC and developed a new code (based on TVD scheme)!!
- The full eigen structure has been derived
- The Jacobian matrix and the eigen structure is derived without assuming any exact form
 of h (EoS)
- This makes the code ideal to compare the effect of various EoS
- For the details of the code and its test runs please see Ryu, Chattopadhyay, Choi (2006)

Highlights of the new code

• The equations of motions in conserved form [$(\rho u^{\nu})_{;\nu}=0,\ T^{\mu\nu}_{;\nu}=0$]:

$$\frac{\partial \vec{q}}{\partial t} + \frac{\partial \vec{F^j}}{\partial x^j} = 0, \tag{v}$$

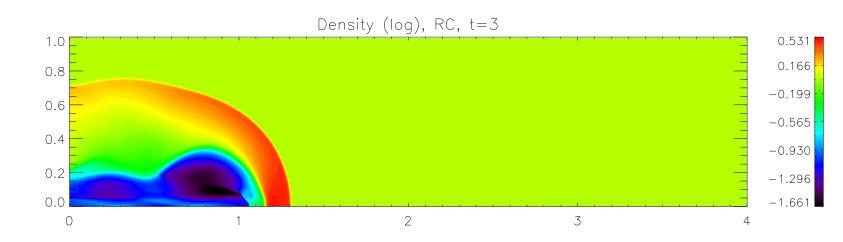
• The conserved quantities are:

$$\vec{q} = \begin{bmatrix} D & M^i & E \end{bmatrix}^T, \qquad \vec{F}^j = \begin{bmatrix} Dv^j & M^iv^j + p\delta^{ij} & (E+p)v^j \end{bmatrix}^T.$$

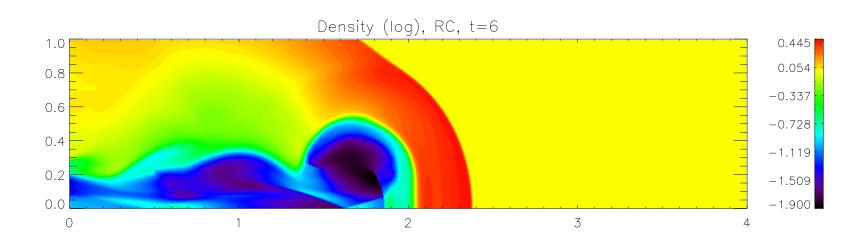
And the transformation relation betⁿ observer frame to fluid rest frame are:

$$D = \Gamma \rho, \quad M^i = \Gamma^2 \rho h v^i, \quad E = \Gamma^2 \rho h - p, \tag{vi}$$

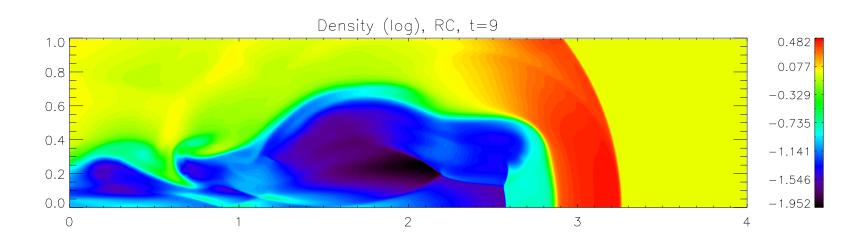
$$\Gamma = (1 + u_i u^i)^{1/2} = 1/(1 - v^2)^{1/2}$$



Jet RC— $log(\rho)$: t=3; Res:1024×256; Y=4X; $X=21.3\times$ jet radii(r_d); Init cond: $v_x=0.9,\, \rho_j=0.1,\, \rho_a=1,\, p=0.01;$ Initial jet length= r_d .

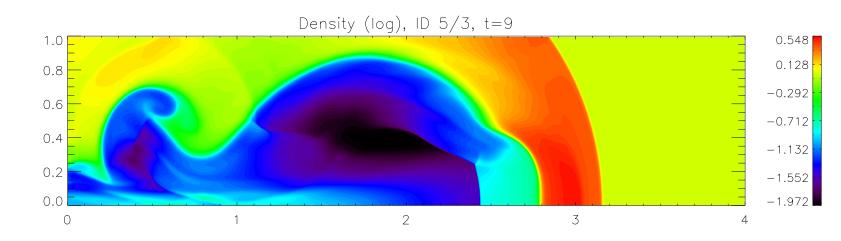


• Jet RC— $log(\rho)$: t=6;

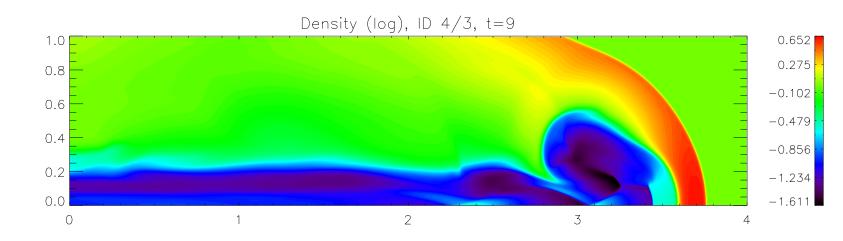


• Jet RC— $log(\rho)$: t=9;

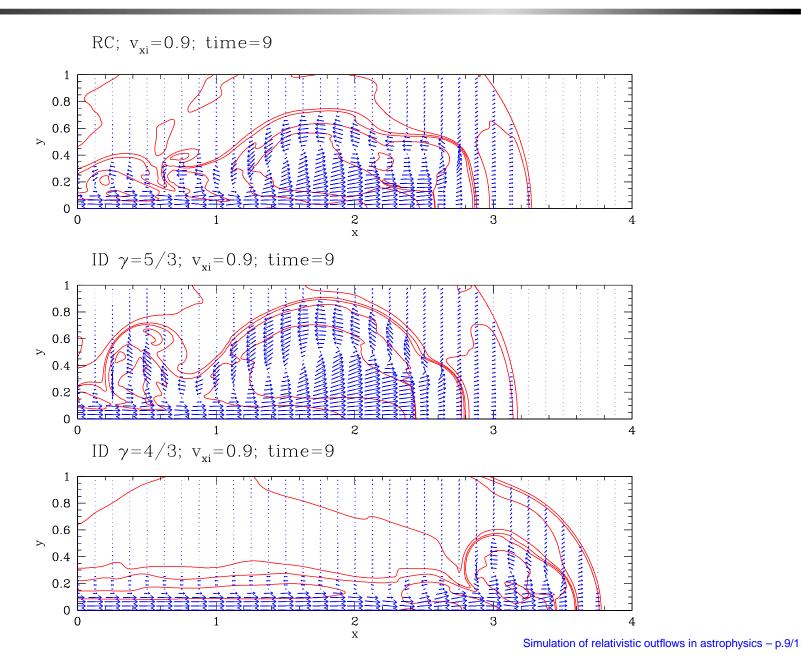
How does solutions with ID EoS look like at this time?



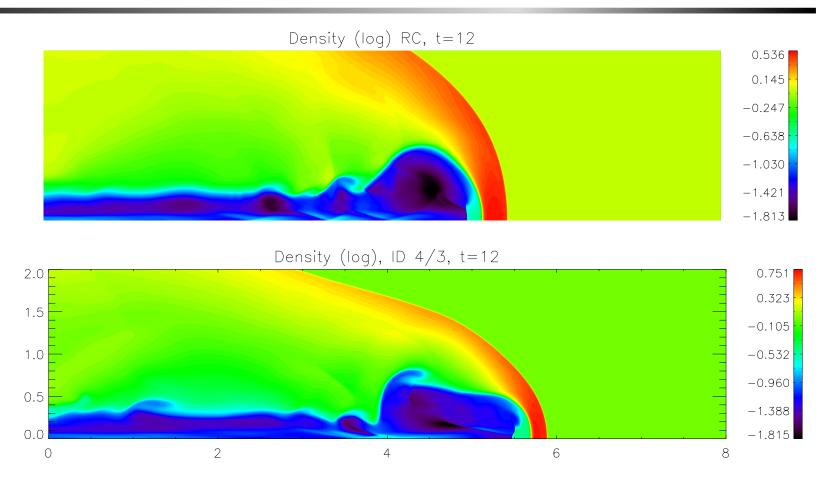
• Jet ID $\gamma = 5/3 - log(\rho)$: t=9; Res:1024×256; Y = 4X; X = 21.3×jet radii(r_d); Init cond: $v_x = 0.9$, $\rho_j = 0.1$, $\rho_a = 1$, p = 0.01; Initial jet length= r_d .



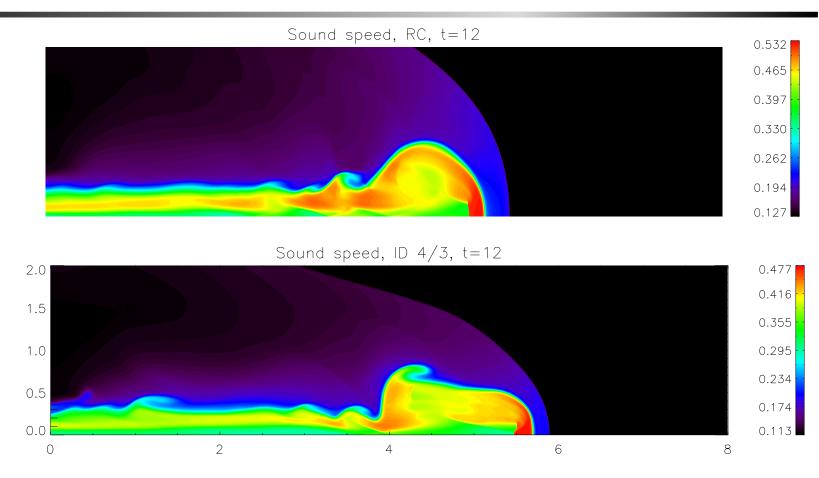
Jet ID $\gamma=4/3$ — $log(\rho)$: t=9; Res: 1024×256 ; Y=4X; $X=21.3\times$ jet radii(r_d); Init cond: $v_x=0.9,\, \rho_j=0.1,\, \rho_a=1,\, p=0.01$; Initial jet length= r_d . ID $\gamma=4/3$ definitely is quite different, but why?



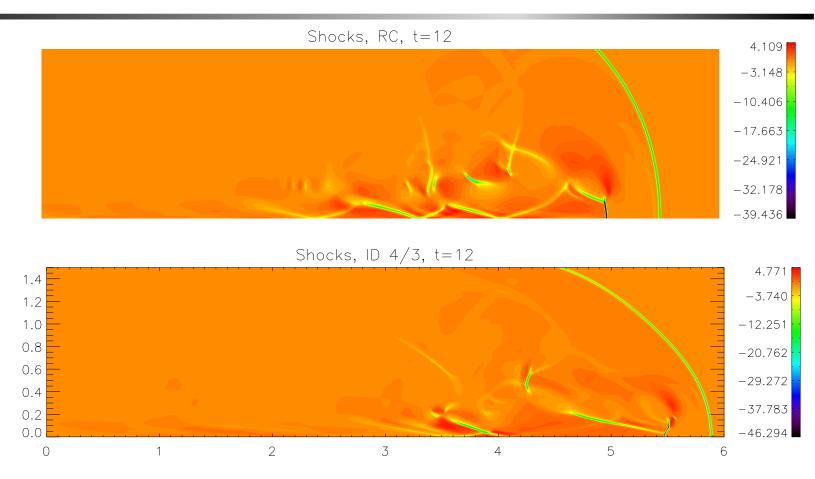
- As jet hits ambient medium it heats up
- A part of it fbws back.
- With ID $\gamma = 5/3$ c_s is higher, it puffs up more, interacts with back fbwing material, instabilities sets in
- With $\gamma = 4/3$, remains thin, limited back reaction, beam structure almost intact!
- With RC correct c_s gives a correct mode of interaction
- ullet The bow shock is in median position between ID $\gamma=5/3$ and $\gamma=4/3$
- ullet With $\gamma=4/3$, even moderate injection Γ , produces near perfect beam structure
- Let us jack up injection velocity



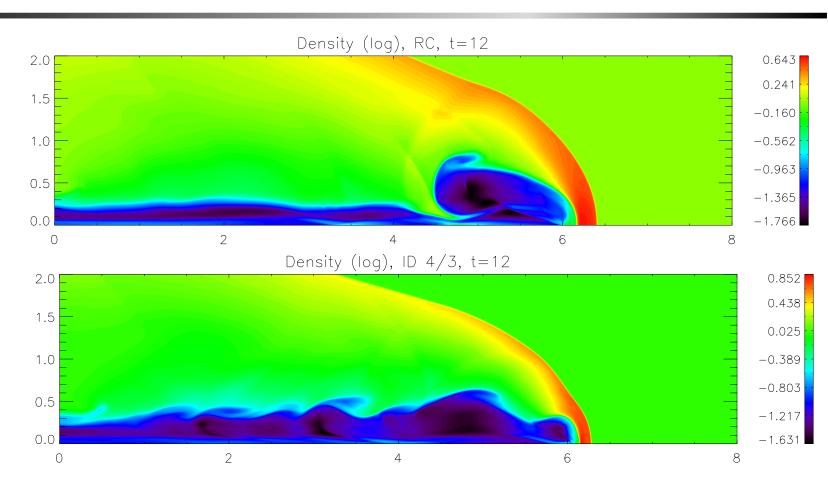
• Density contours at t=12. Upper panel RC, lower panel ID ($\gamma=4/3$), $v_{xi}=0.95$.



• Sound speed at t=12. Upper panel RC, lower panel ID $(\gamma=4/3)$, $v_{xi}=0.95$.

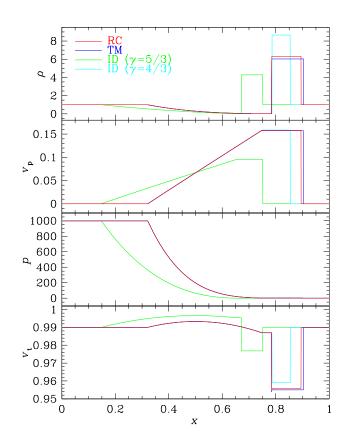


Shocks at t = 12. Upper panel RC, lower panel ID ($\gamma = 4/3$), $v_{xi} = 0.95$. Should affect emitted radiation.



t = 12; Density: $v_{xi} = 0.96$;

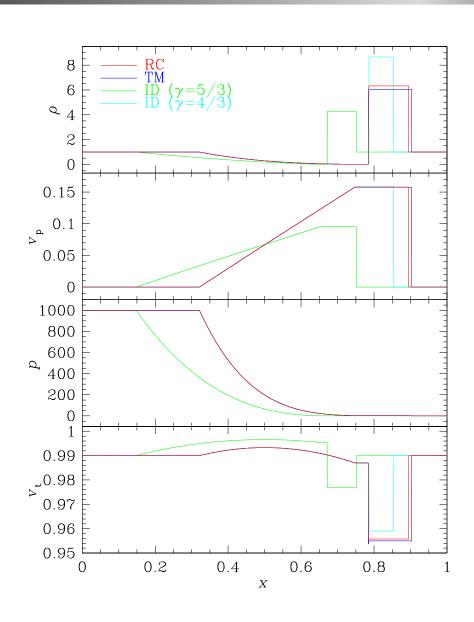
solution with RC is faster!!!



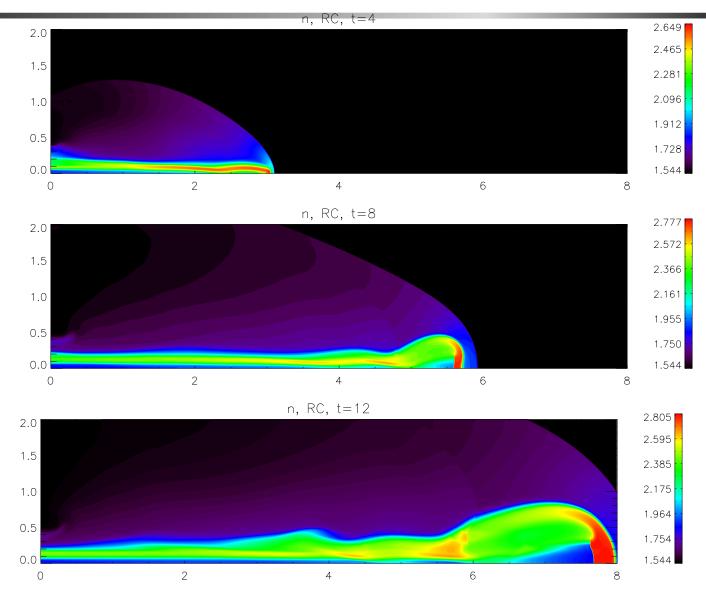
Strong-Shock Tube — t=0.18; Init cond:

$$(\rho, v^x, v^y, v^z, p) = (1, 0, 0.99, 0, 10^3); 0 \le x \le 0.5$$

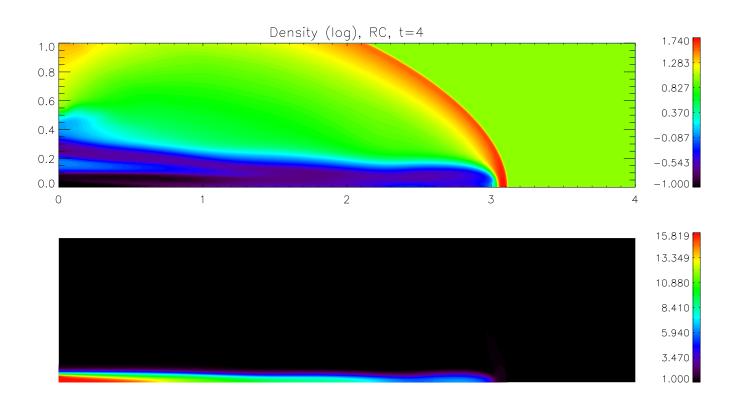
= $(1, 0, 0.99, 0, 10^{-2}); 0.5 < x \le 1.$



• Using ID EoS and some intermediate values of γ is not good, since γ generated by the interaction of the outflow with the the ambient medium



RC: $v_{xi} = 0.99$: n is variable and is neither 3 nor 3/2



• RC $v_{xi}=0.998$, upper panel density and lower panel Γ

Concluding Remarks

- ID EoS is relativistically wrong.
- Considering temperature dependent adiabatic/polytropic index is important.
- Internal structure produced by RC is different.
- These internal shocks will produce a different spectrum.
- Injection variables derived by analyzing observational data will also be faulty if wrong EoS is chosen.
- The jet head moves slower or faster than that modeled by ID EoS.
- Adiabatic index depends on the thermodynamic properties of the jet, which in turn is determined by the complicated interaction with the ambient medium, thus cannot be assigned apriori.
- Our preliminary investigation suggests, it will be interesting to investigate
 propagation of jets through non uniform medium.